

Outcome of RMR Determination, MRA Evaluation Process and Methodology - Transmission Planning in ERCOT

ERCOT Transmission Planning

November 16, 2018

Timeline of Overall Process



* Per ERCOT Nodal Protocol Section 3.14.1.2(9), the RMR or MRA agreement may be executed after the 150 or 90 days period.



Outcome of RMR Determination

- Within 60 days, ERCOT completes its reliability analysis and issues a market notice describing the results of its reliability analysis
- □ If it is determined that the proposed suspension of the Generation Resource would result in a performance deficiency (Criteria: Nodal Protocol Section 3.14.1.2), then within 10 days after the final assessment, ERCOT shall issue a Request for Proposals (RFP) for Must-Run Alternatives (MRAs).
- ERCOT shall include in the RFP reasonably available information that would enable potential MRAs to assess the feasibility of submitting a proposal



Key Information Available in RFP (NPRR896)

□ ERCOT shall specify the following information in the RFP.

- <u>Expected number of hours</u> that an MRA would be needed during the contract period, and <u>the hours of the day</u>, <u>by season</u>, that the MRA would be required to be available.
 - Study case and historical weather data will be used to estimate the information. More details are in the next slides
- <u>Shift factors</u> associated with each bus where potential MRA would help relieve performance deficiency. Shift factors can be used for determining the approximate <u>capacity</u> of potential MRA Resources.
 - Study case will be used to calculate shift factors.



Methodology to Estimate Hours, Days, and Seasons

- Suppose that an RMR study was done using a summer peak case and identified criteria violations.
 - Step 1

RMR Study Case(s)



Estimate critical load level with no criteria violations

- i. Reduce the load in the area of concern until there is no criteria violation to identify a load level with no criteria violations.
- ii. Suppose it is found that the critical load level without any criteria violations is 24,362 MW for the study area.



- i. Study area load(s) forecasted using historical weather data.
- ii. Identify hours, dates, and seasons above the critical load level, i.e. 24,362 MW in Step 1



Example – Expected Number of Hours above Critical Load Level

Weather Year	Number of hours (Load Level ≥ Critical Load Level)
2011	38
2012	55
2013	44
2014	47
2015	13
2016	31
2017	27
Average	37





Example – Expected Days, Hours, and Season



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Example – Shift Factors for Estimating Capacity

on	Substatio	Load Zone	Shift Factor	Area Name	Area Num	Name	Bus Number
EN	ZE	LZ_HOUSTON	-19.0%	CNP_TSP	4	ZENITH345A	44900
EN	ZE	LZ_HOUSTON	-18.3%	CNP_TSP	4	ZENITH138A	44910
RY	FF	LZ_HOUSTON	-18.1%	CNP_TSP	4	FRYRD09_138X	45812
EN	ZE	LZ_HOUSTON	-18.1%	CNP_TSP	4	ZENITH_A1TER	49085
EN	ZE	LZ_HOUSTON	-18.1%	CNP_TSP	4	ZENITSTR	44901
RY	FF	LZ_HOUSTON	-18.0%	CNP_TSP	4	FRYRD76_138X	45811
GE	(LZ_HOUSTON	-18.0%	CNP_TSP	4	GERTIE218000	45801
GE	(LZ_HOUSTON	-17.9%	CNP_TSP	4	GERTIE768010	45802
CYF	C`	LZ_HOUSTON	-17.7%	CNP_TSP	4	CYFAIR218035	45711
IW	TH	LZ_HOUSTON	-17.7%	CNP_TSP	4	T_H_W345B	45500
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	T_H_WSTR	45503
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	T_H_WSTR	45504
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	T_H_WSTR	45505
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT51	110052
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT52	110053
łW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT53	110054
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT54	110055
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT55	110056
IW	TH	LZ_HOUSTON	-17.7%	E_CNP_TSP	904	THW_THWGT56	110057
łW	TH	LZ_HOUSTON	-17.5%	CNP_TSP	4	T_H_WA3TER	49071
łW	TH	LZ_HOUSTON	-17.5%	CNP_TSP	4	T_H_WSTR	45502
KL		LZ_HOUSTON	-17.4%	CNP_TSP	4	CKLUGE_138A	45953
CYF	C`	LZ_HOUSTON	-17.4%	CNP_TSP	4	CYFAIR768030	45712
KI		LZ_HOUSTON	-17.4%	CNP_TSP	4	KLEIN138A	45940
KL		LZ_HOUSTON	-17.4%	CNP_TSP	4	KLUGE138B	45952
IW	TH	LZ_HOUSTON	-17.4%	CNP_TSP	4	T_H_W138A	45510
w	TH	LZ_HOUSTON	-17.4%	CNP_TSP	4	T_H_W95_8265	45512
LO	WL	LZ_HOUSTON	-17.4%	CNP_TSP	4	WILLOW_8010	46660
ΒA	E	LZ_HOUSTON	-17.3%	CNP_TSP	4	BAMMEL_138A	45651
CI		LZ_HOUSTON	-17.3%	CNP_TSP	4	CAMRON_138A	45700
JES	JI	LZ_HOUSTON	-17.3%	CNP_TSP	4	JESTER678030	45921
JES	JI	LZ_HOUSTON	-17.3%	CNP_TSP	4	JESTER818000	45922
IW	TH	LZ_HOUSTON	-17.3%	CNP_TSP	4	T_H_W_A1TER	49039
łW	TH	LZ HOUSTON	-17.3%	CNP TSP	4	T H WSTR	45501
/ET	VI	LZ HOUSTON	-17.3%	CNP TSP	4	VETRAN678020	46551
/ET	VI	LZ_HOUSTON	-17.3%	CNP_TSP	4	VETRAN818005	46552
GZ	(LZ_HOUSTON	-17.2%	CNP_TSP	4	GEARS95_8030	45782
ΗV	H	LZ_HOUSTON	-17.2%	CNP_TSP	4	HIDDEN958015	45862
IW	TH	LZ_HOUSTON	-17.2%	CNP_TSP	4	T_H_W138E	45515
łW	TH	LZ_HOUSTON	-17.2%	CNP_TSP	4	T_H_W81_8090	45511
łW	TH	LZ HOUSTON	-17.2%	E CNP TSP	904	T H WSTR	45516

Shift factor at this location is approximately negative 19% to the constraint under contingency.

If 100 MW of capacity can be injected from an MRA available at this location, it would reduce the flow on the overloaded element by approximately 19 MW.

This will help prospective MRA resource(s) estimate capacity needed at each location or combinations of locations.

MRA Evaluation Process and Methodology - Transmission Planning in ERCOT



RMR and MRA Evaluation Process – ERCOT Planning

<Example of Cost Comparison>

		Options	Bidding Cost (\$)	Cost of Load at Risk (\$)	Total Cost (\$)
MRA A, MRA B, MRA C, , MRA K	• Review Eligibility	MRA B	20	-	20
	 Reliability Analysis and 	MRA D	25	10	35
	Load Shedding Analysis	MRA E + MRA K	15	3	18
	Cost Analysis	RMR	30	-	30
		Do-Nothing	-	20	20



Methodology to Estimate Cost of Load at Risk



Cost of Load at Risk = Probability of Contingency x VOLL x MW Load at Risk X Expected Number of Hours

Formula – Cost of Load at Risk

Cost of Load at Risk =

$$P_{n0} * \sum_{all i} (VOLL * L_i * H_i) + P_{n1} * \sum_{all j} (VOLL * L_j * H_j) + \sum_{all k} \left(P_k * \sum_{all s1} VOLL * (L_{k,s1} * H_{k,s1}) \right) + \sum_{all l} \left(P_l * \sum_{all s2} VOLL * (L_{l,s2} * H_{l,s2}) \right)$$

Where,

- P_{n0} is the probability of shedding load under pre-contingency condition (i.e. $P_{n0} = -1.0$)*,
- P_{n1} is the probability of shedding load under N-1 contingency condition (i.e. $P_{n1} = -1.0$)*,
- P_k is the probability of shedding load under the prior outage of kth G-1 in anticipation of next N-1 contingency (i.e. P_k= probability of G-1),
- *P_l* is the probability of shedding load under the prior outage of *lth* X-1 in anticipation of next critical N-1 contingency (i.e. *P_l* = probability of X-1),
- VOLL is the value of lost load (i.e. \$ 9,000 / MWh),
- *L* is the MW load at risk under each contingency condition,
- *H* is the hours with load at risk load under each contingency condition,
- *i*, *j*, *s*₁ and *s*₂ are the assumed number of incremental load shedding levels
- *o* and *x* are the total number contingency causing RMR criteria violations under G-1 or X-1

Note: Probability of shedding load under N-0 and N-1 was assumed to be approximately 1.0 based on the assumption that the load shedding for critical N-0 and N-1 issues would occur under pre-contingency condition.



Suppose that an NSO was submitted for the retirement starting from Jan 2018. RMR Study was conducted using the 2018 summer peak case which has 25,362 MW of peak load in the study area. Suppose that we identified two G-1+ N-1 contingencies causing criteria violations.



Step 1: Load Shedding Analysis for Do-Nothing Option or MRA(s) that partially address criteria violations.

 Load Shedding Analysis was performed and it was found that the load in the study area needs to be reduced as follows under each of the two contingencies

a) Contingency 1 (G_1 -1 + N-1) needs 1000 MW load shedding to eliminate the criteria violations

25,362 MW - 24,362 MW = 1000 MW

b) Contingency 2 (G_2 -1 + N-1) needs 500 MW load shedding to eliminate the criteria violations

25,362 MW - 24,862 MW = 500 MW





Step 2: Review Study Area Load Forecast

 Expected number of hours with criteria violations can be obtained using the critical load level and based on the review of study area loads forecasted using historical weather data

Weather Year	Number of hours (Study Area Load ≥ 24,862 MW Critical Load Level)	Number of hours (Study Area Load ≥ 24,362 MW Critical Load Level)
2011	10	38
2012	17	55
2013	8	44
2014	15	47
2015	3	13
2016	12	31
2017	18	27
Average	12	37

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Step 3: Compute Cost of Load at Risk

- Assume the probability of generator outage associated with Contingency 1: 0.00065664
- Assume the probability of generator outage associated with Contingency 2: 0.004877
- Value of Lost Load (VOLL): \$9,000 per MWhr
- Now, use formula to compute the cost of load at risk
- If more accuracy is desired, split the range of critical load level into multiple levels. For example, split the range of the critical load level into two incremental ranges (i.e. 25,362 ~ 24,862 MW and 24,862 ~ 24,362 MW) for Contingency 1. Then, the amount of load at risk at each incremental range is
 - The amount of load shedding for the first range =

1000 MW / 2 =500 MW for 12 hours

the amount of load shedding for the second range =

1000 MW / 2 = 500 MW for 37 hours

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Expected Cost of Load at Risk for contingency $\mathbf{1} = P_1 * \sum_{s_1=1}^{q} VOLL * (L_{1,s_1} * H_{1,s_1})$ = 0.00065664 * (9,000 * 500 * 12 + 9,000 * 500 * 37) = \$144,789

Expected Cost of Load at Risk for contingency $\mathbf{2} = P_2 * \sum_{s_1=1}^{q} VOLL * (L_{1,s_1} * H_{1,s_1})$ = 0.004877 * (9,000 * 500 * 12) = \$263,358

For this example, the cost of load at risk associated with Do-Nothing option can be estimated as follows:

= Cost of Load at Risk Under Contingency 1 + Cost of Load at Risk Under Contingency 2

= \$144,789 + \$ 263,358 = <mark>\$408,147</mark>







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Appendix





Reference for VOLL:

"Methodology for Implementing ORDC to Calculate Real-Time Reserve Price Adder" available at <u>http://www.ercot.com/mktrules/obd/obdlist</u>

