

Primary Frequency Response (PFR)/Fast Frequency Response(FFR) Assessment

ERCOT Future Ancillary Service Team

ERCOT FAST Workshop

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Preliminary

Background and Purpose

- Background:
 - The Future Ancillary Service Team (FAST) has discussed concepts and proposals for a new framework for Ancillary Services in ERCOT.
 - ERCOT was asked in the FAST working sessions to provide an indication of the quantities that might be required for the proposed Ancillary Services.
- Purpose:
 - To "estimate" the PFR/FFR needs (in terms of MW) under different system conditions.
 - This results of this assessment only provide a reference for ERCOT FAST consideration. The assumptions made in this assessment were based on the proposed AS framework and should not be used for other purposes.



Definition

- Primary Frequency Response (PFR):
 - The immediate proportional increase or decrease in real power output provided by a Resource and the natural real power dampening response provided by Load in response to system frequency deviations. This response is in the direction that stabilizes frequency.
- Fast Frequency Response (FFR):
 - A response from a resource that is automatically self-deployed and provides a full response within 30 cycles after frequency meets or drops below a preset threshold.
 - Two FFR subgroups:
 - FFR1: trigger frequency at 59.8 Hz
 - FFR2: trigger frequency at 59.7 Hz
- PFR and FFR help to stabilize the frequency but do not recover the frequency back to nominal frequency.



Study Assumptions and Criteria

- Study Assumptions
 - Only PFR units provided governor response
 - Non-PFR units were assumed at their physical limit, no headroom to provide governor response.
 - Load damping was assumed as 2%/Hz based on PDCWG data
 - No Wind Dynamic Model
 - Two subgroups of FFR service, at different frequency thresholds
 - FFR1: 59.8 Hz, FFR2: 59.7 Hz
- Study Criteria and contingency
 - Freq nadir >= 59.4 Hz, losing two STPs
 - Freq overshoot <=60.5 Hz, losing one unit and triggering all FFR deployments
- Study Cases
 - Multiple system conditions



2013 Net Load (= load - wind)





Selected Study Cases

							System
			Wind		Wind		Inertia***
		Load	Output	PRC*	Penetration	Net Load	(GW-
Case	Date/Time	(MW)	(MW)	(MW)	* *	(MW)	Second)
	08072013						
1	17:00	67,148	2,398	4,105	3.57%	64,750	372
	02132014						
2	19:00	36,460	1,188	5 <i>,</i> 062	3.26%	35,272	236
	01132014						
3	03:00	24,857	7,196	5,812	28.95%	17,661	174

*PRC: Physical Reserve Capacity

**Wind Penetration = Wind output / Load

***System Inertia (GW-second) = Sum of (Machine MVA * H) / 1000



Study Approach

- Detailed dynamic simulations were performed in this assessment to evaluate the system frequency response in the first 20~30 seconds following a frequency events.
- This assessment included the impact of the following proposed Ancillary Services.
 - Synchronous Inertial Response
 - Primary Frequency Response
 - Fast Frequency Response



Questions to Answer

- Why do we need PFR and FFR?
- Do the PFR and FFR requirements vary with system conditions?
- What are the preliminary estimated requirements for PFR and FFR?
- What is the relationship between PFR and FFR?



Test 1: No PFR, No FFR, System Inertia (SI) Only



Test 1: No PFR, No FFR, System Inertia Only



RoCoF: Rate of Change of Frequency

RoCoF (Hz/sec): 1 < 2 < 3



Test 2: Minimum PFR Needs

- Test: all three cases
- Target:
 - Frequency nadir >= 59.4 Hz with the loss of two STP units
- Assumptions
 - Only PFR units provided governor response
 - Non-PFR units were assumed at their physical limit, no headroom to provide governor response.
 - Load damping was assumed as 2%/Hz based on PDCWG data
 - No Wind Dynamic Model
 - No FFR



Test 2: Simulation Results



Test 3: Minimum FFR Needs

- A minimum PFR capacity is required to identify the minimum FFR needs.
- Criteria to determine the minimum PFR
 - Potential # of FFR deployments in a year
 - Frequency nadir >= 59.7 Hz with the loss of one generation unit
- Results: a minimum of 1,400 MW of PFR was needed

	Load		Frequency Nadir	Generation
Date/Time	(MW)	PFR (MW)	(hz)	Loss (MW)
08072013 17:00	67,148	1,400	59.70	1,350
02132014 19:00	36,460	1,400	59.70	950
01132014 03:00	24,857	1,400	59.70	350



Test 3: Simulation Results



Test 4: FFR Impact at High Load

- What is the FFR contribution at high load?
 - Having only PFR in the high load condition results in a low postdisturbance frequency (Point B).
 - May require additional regulation and contingency reserve to recover the frequency back to 60 Hz.



Test 4: FFR Impact at High Load





Test 5: PFR/FFR Substitution

- Test: all three cases
- Target:
 - Obtain sufficient PFR + FFR_(59.8Hz) + FFR_(59.7Hz)
 - Frequency nadir >= 59.4 Hz with the loss of two STP units
- Assumptions
 - Only PFR units provided governor response
 - Non-PFR units were assumed at their physical limit, no headroom to provide governor response.
 - Load damping was assumed as 2%/Hz based on PDCWG data
 - No Wind Dynamic Model



Test 5: Simulation Results for Case 3



Preliminary

Answers to Questions

• Why do we need PFR and FFR?

To maintain adequate frequency response following an event.

- Do the PFR and FFR requirements vary with system conditions?
 - Yes, PFR/FFR requirements vary with system conditions.
- What are the preliminary estimated requirements for PFR and FFR?
- What is the relationship between PFR and FFR?

Case	Net Load (GW)	PFR _{min} (MW)	FFR _{min} (MW)	PFR/FFR Substitution*
1	65	1,400	0	0
2	35	1,400	700	1.5
3	18	1,400	1,400	2.35

* PFR MWs that can be "replaced by" 1 MW FFR, based on the assumptions in the Case

