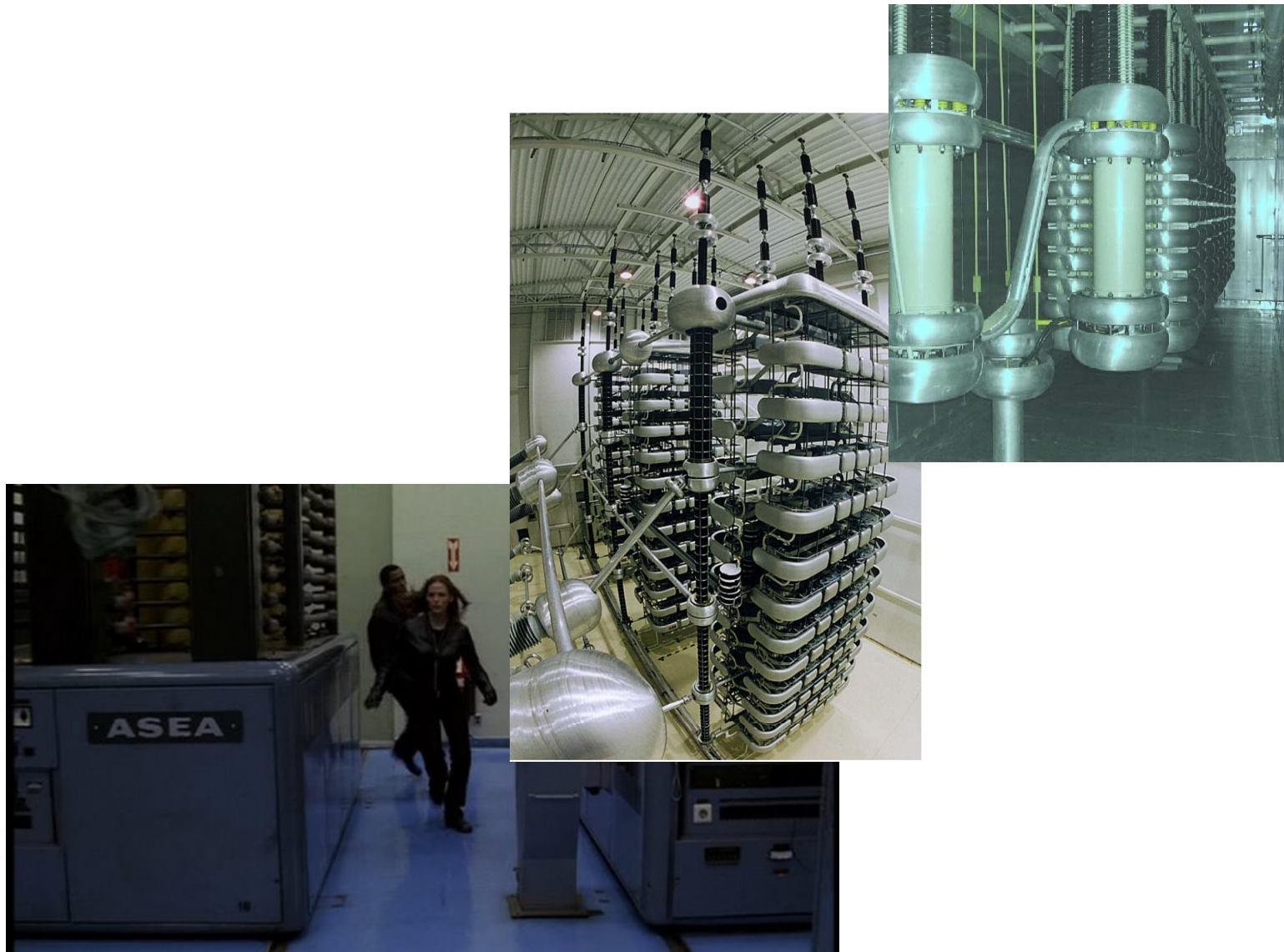


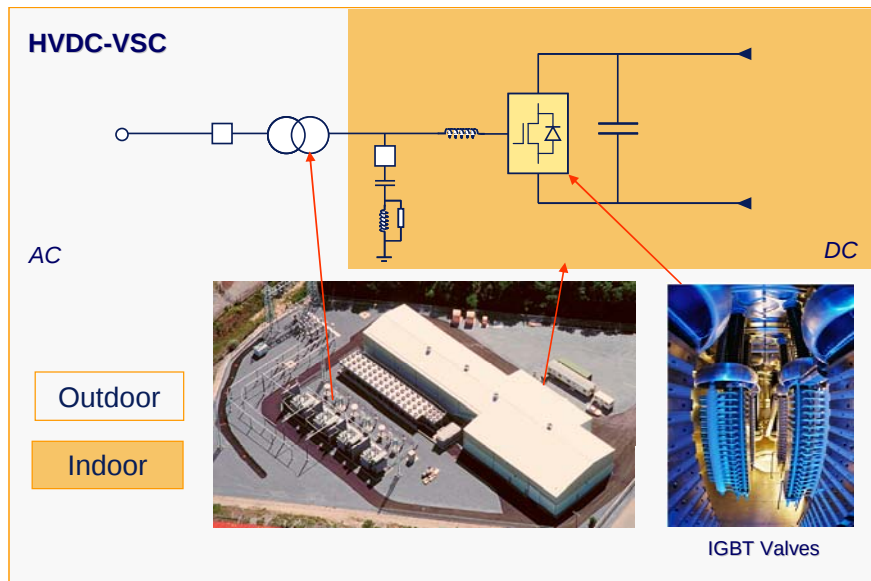
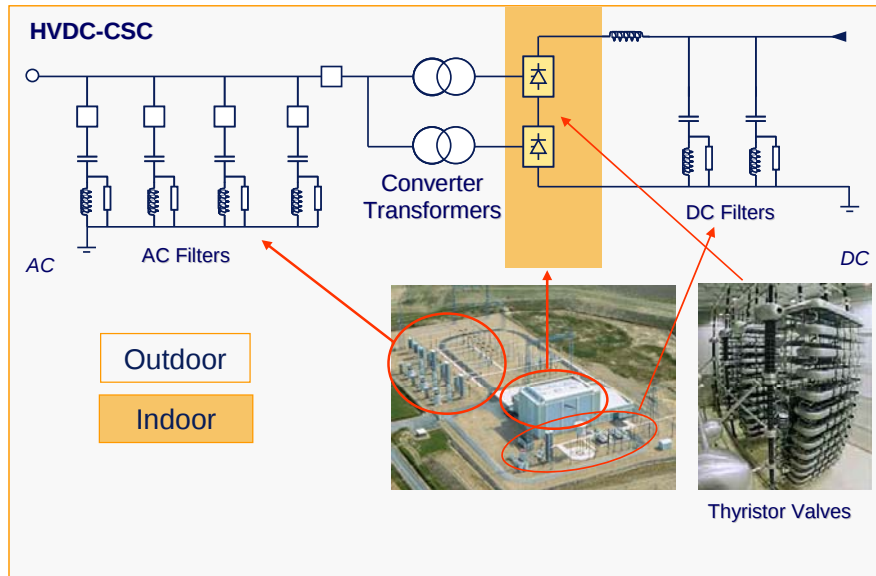
Topics

- HVDC Fundamentals
 - Conventional Converters
 - Capacitor Commutated Converters
 - Voltage Source Converters
 - Reactive Power Requirements
 - System Configurations
 - Tapping
 - Control basics
 - High Power Transmission

Evolution . . .



Core HVDC Technologies



■ HVDC Classic

- Current source converters
- Line-commutated thyristor valves
- Requires 50% reactive compensation (35% HF)
- Converter transformers
- Minimum short circuit capacity > 2x converter rating

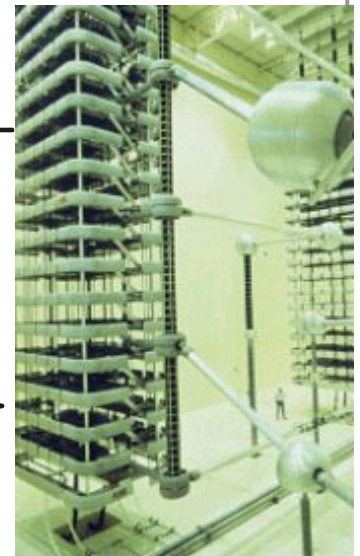
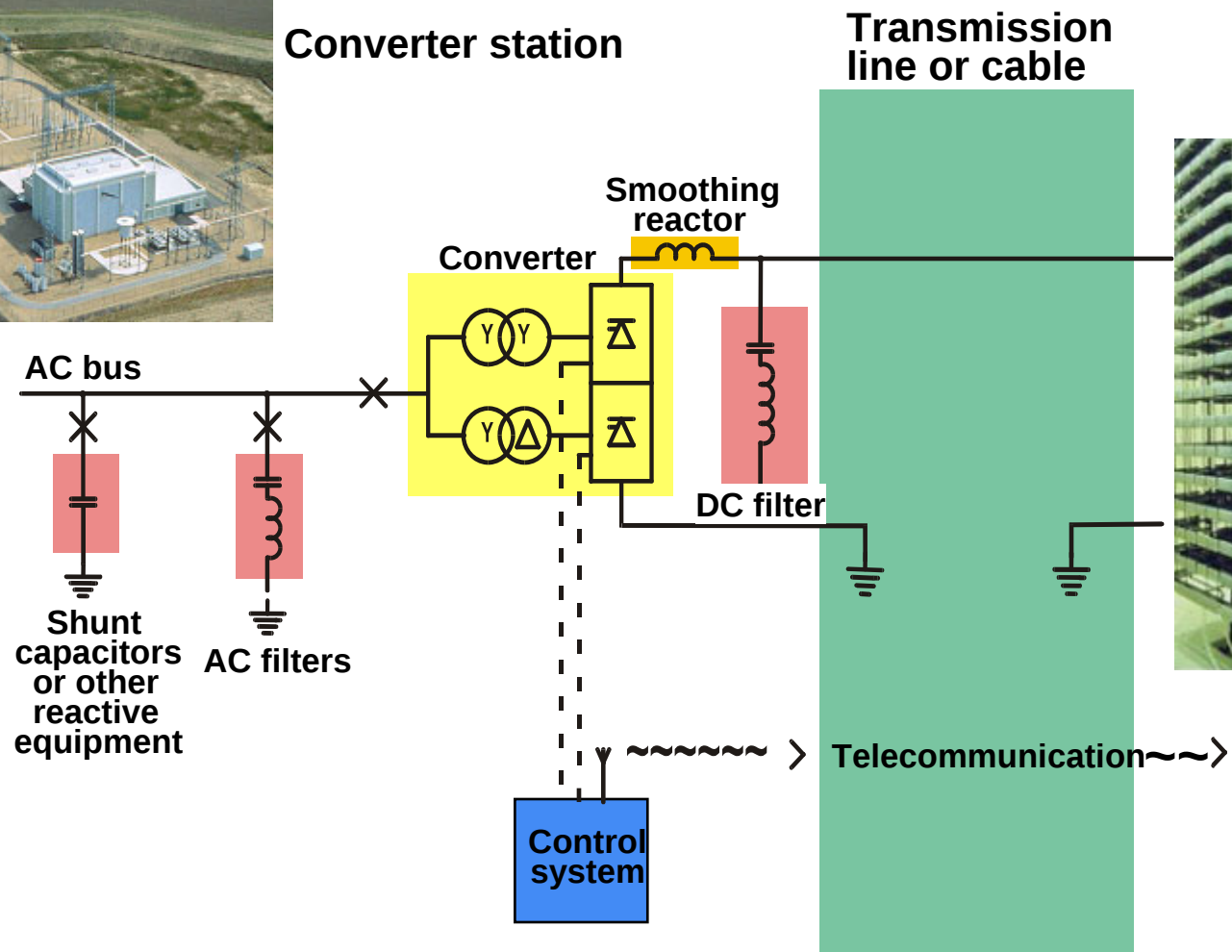
■ HVDC Light

- Voltage source converters
- Self-commutated IGBT valves
- Requires no reactive power compensation (15% HF)
- Standard transformers
- No minimum short circuit capacity, black start

The HVDC Classic Converter Station

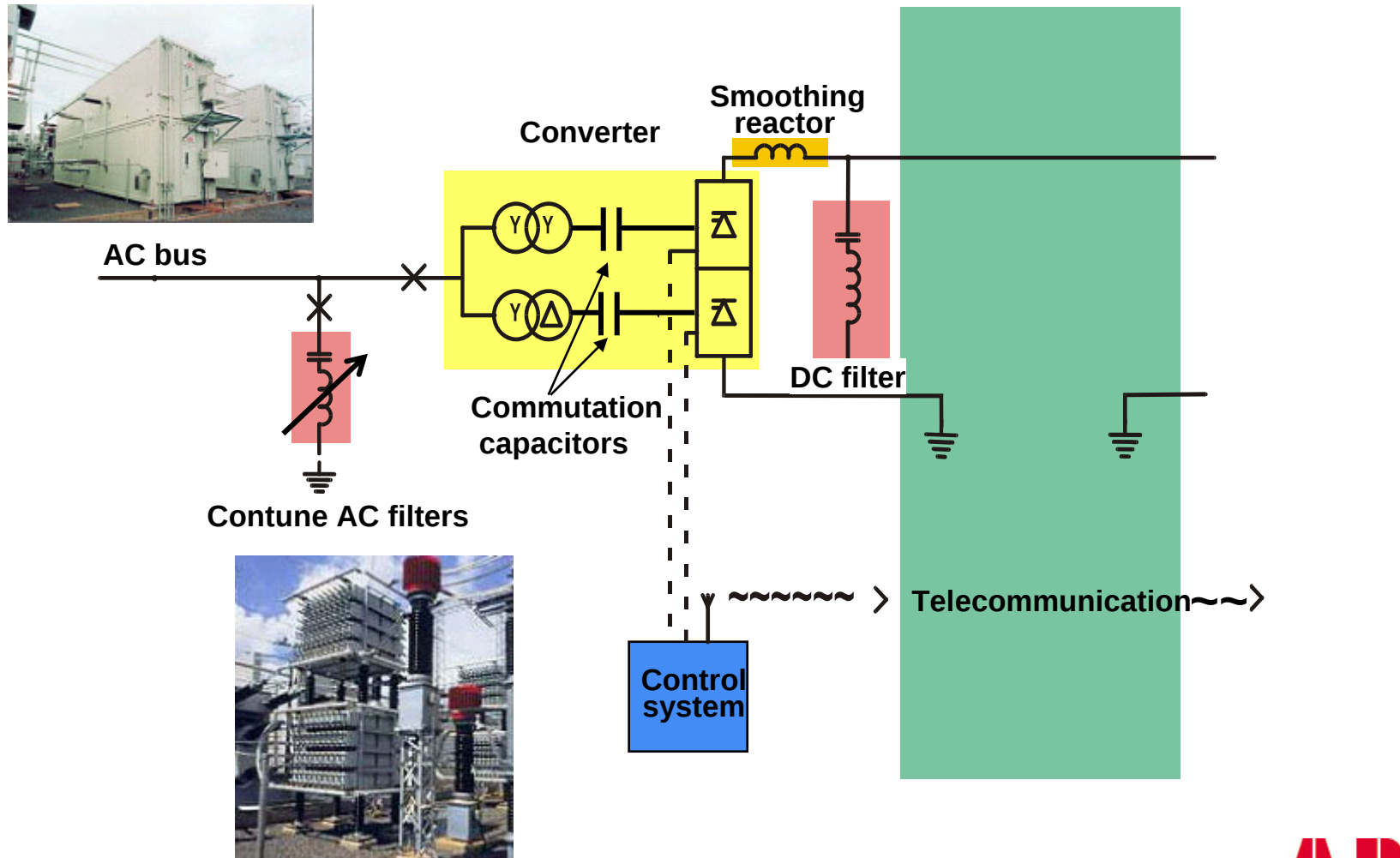


Converter station

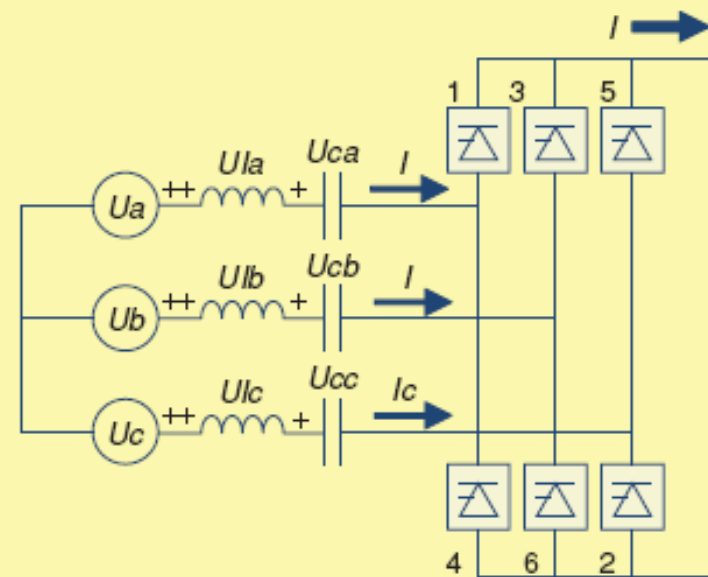
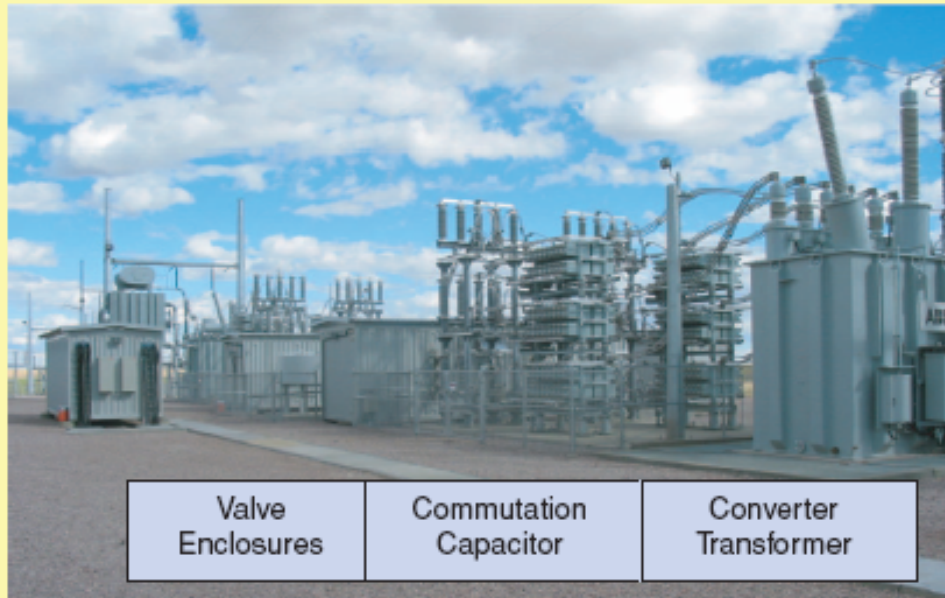


The CCC* Station

*Capacitively-commutated converter

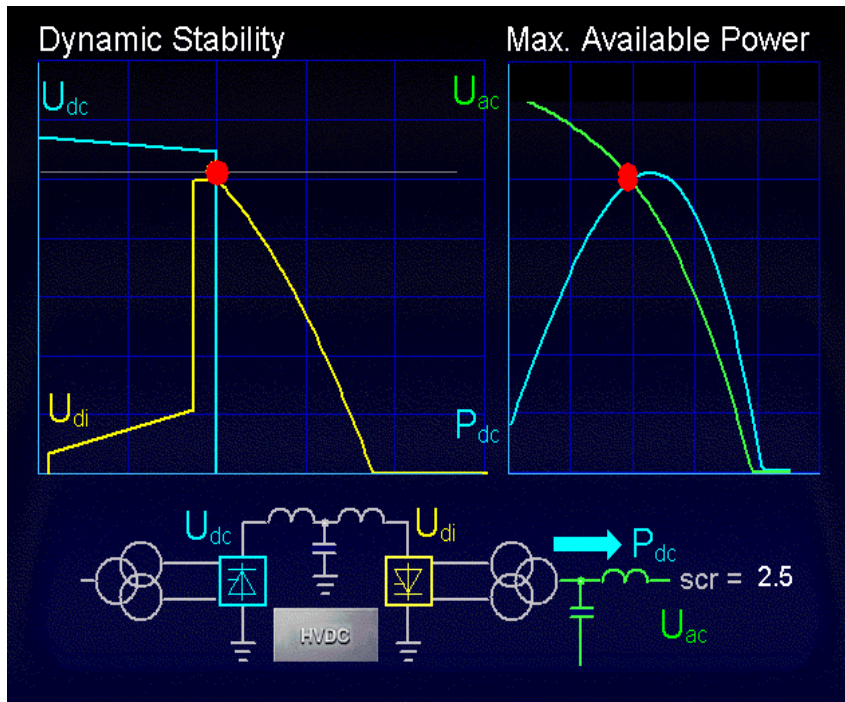


Modular Back-toBack CCC Asynchronous Tie

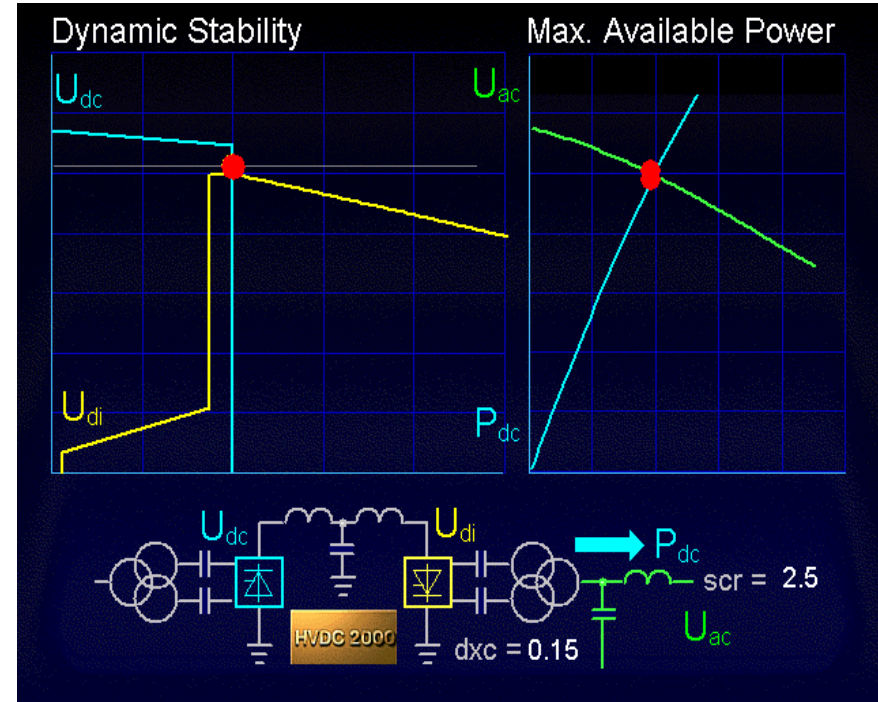


Improved Stability and Higher Power Transfer

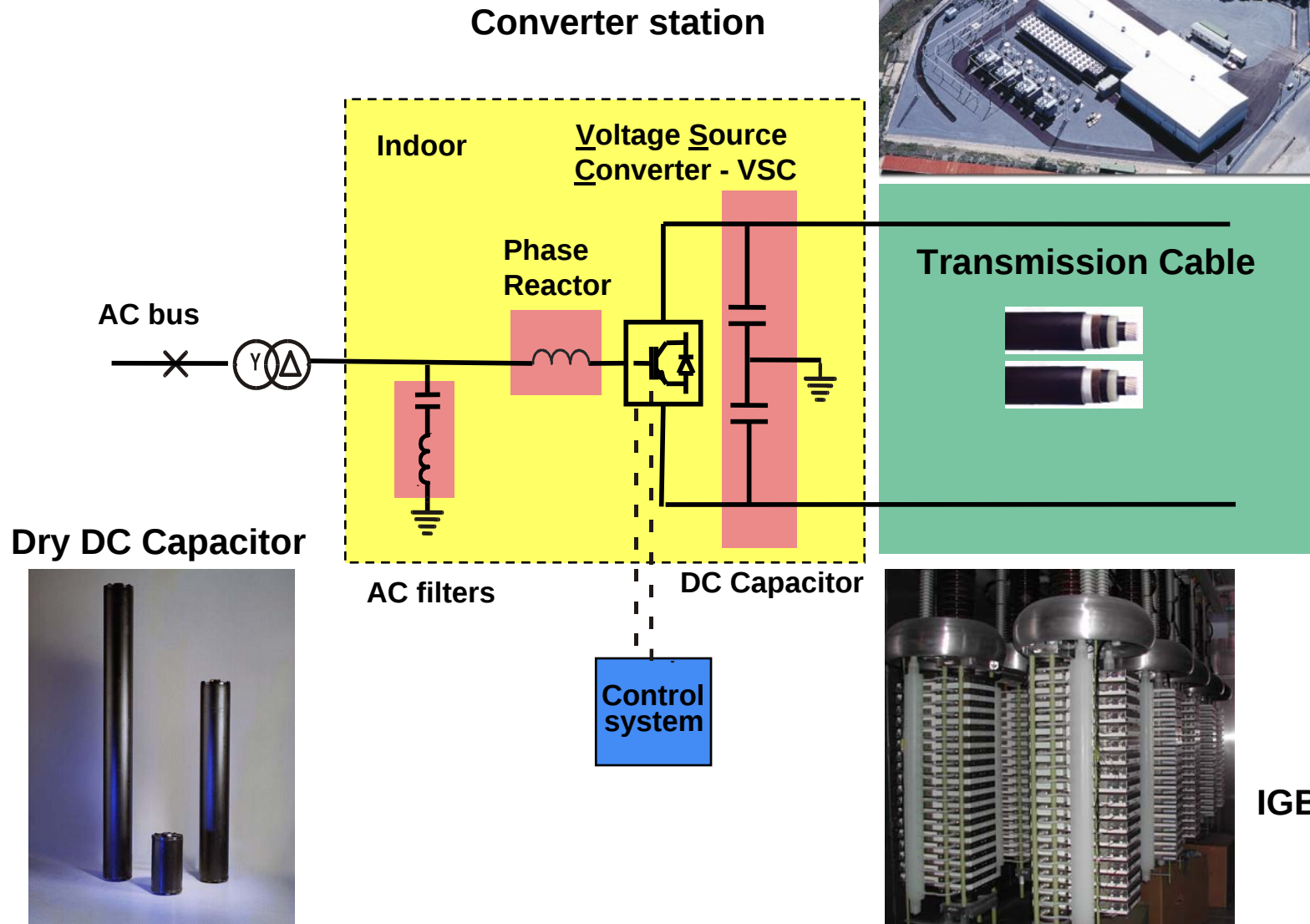
HVDC Classic



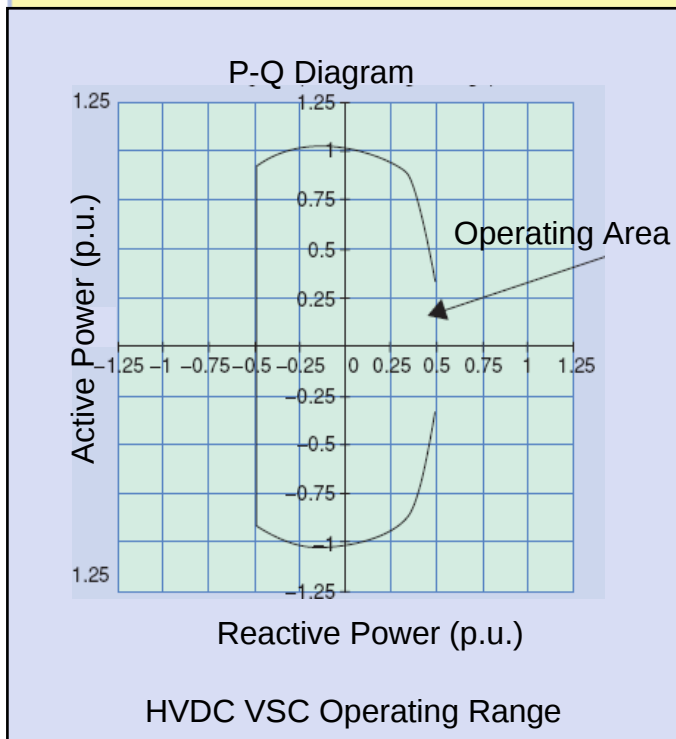
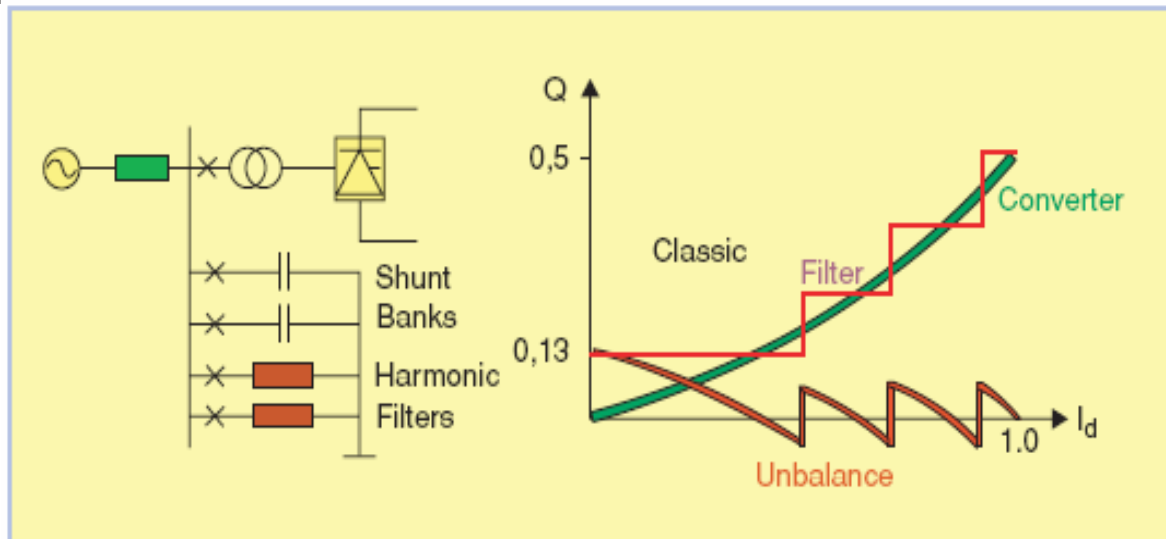
HVDC CCC



The HVDC Light Converter Station

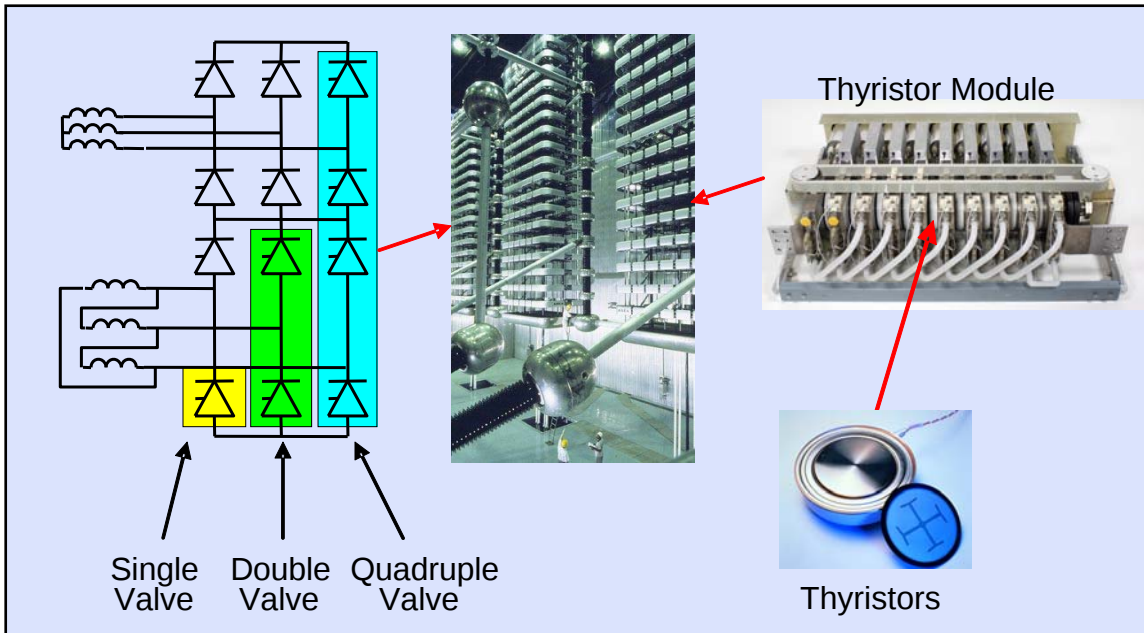


Comparison of Reactive Power Characteristics



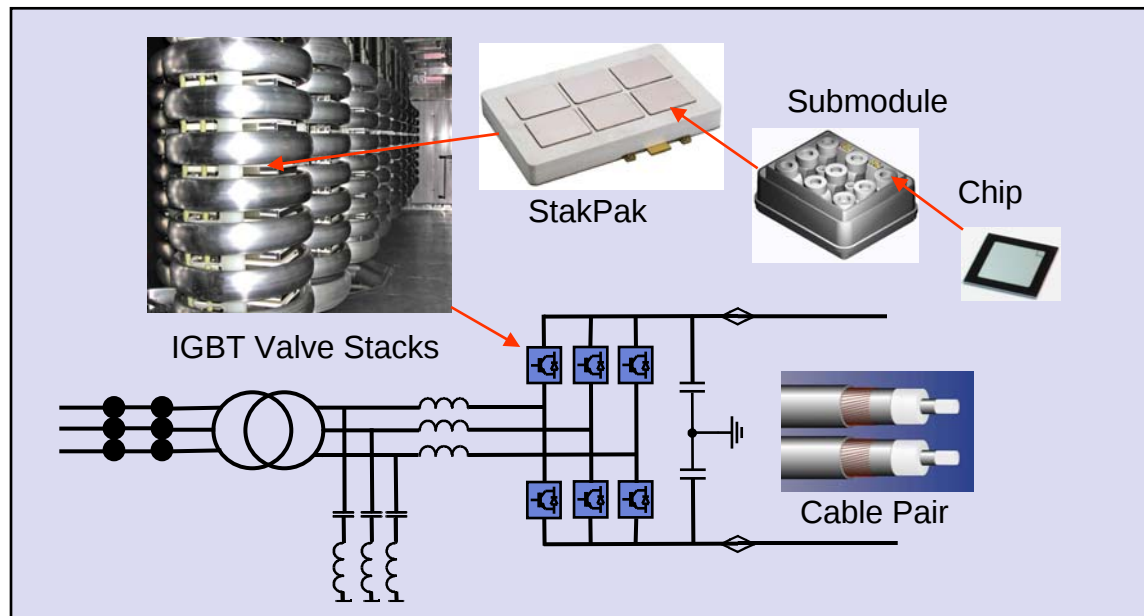
- Conventional HVDC – HVDC Classic
(~ SVC with TCR+FC, $-0.5P_d$ / $+0$ MVar)
- VSC Based HVDC – HVDC Light
(~ STATCOM, $-0.5P_d/+0.5P_d$ MVar)

HVDC Converter Arrangements



HVDC Classic

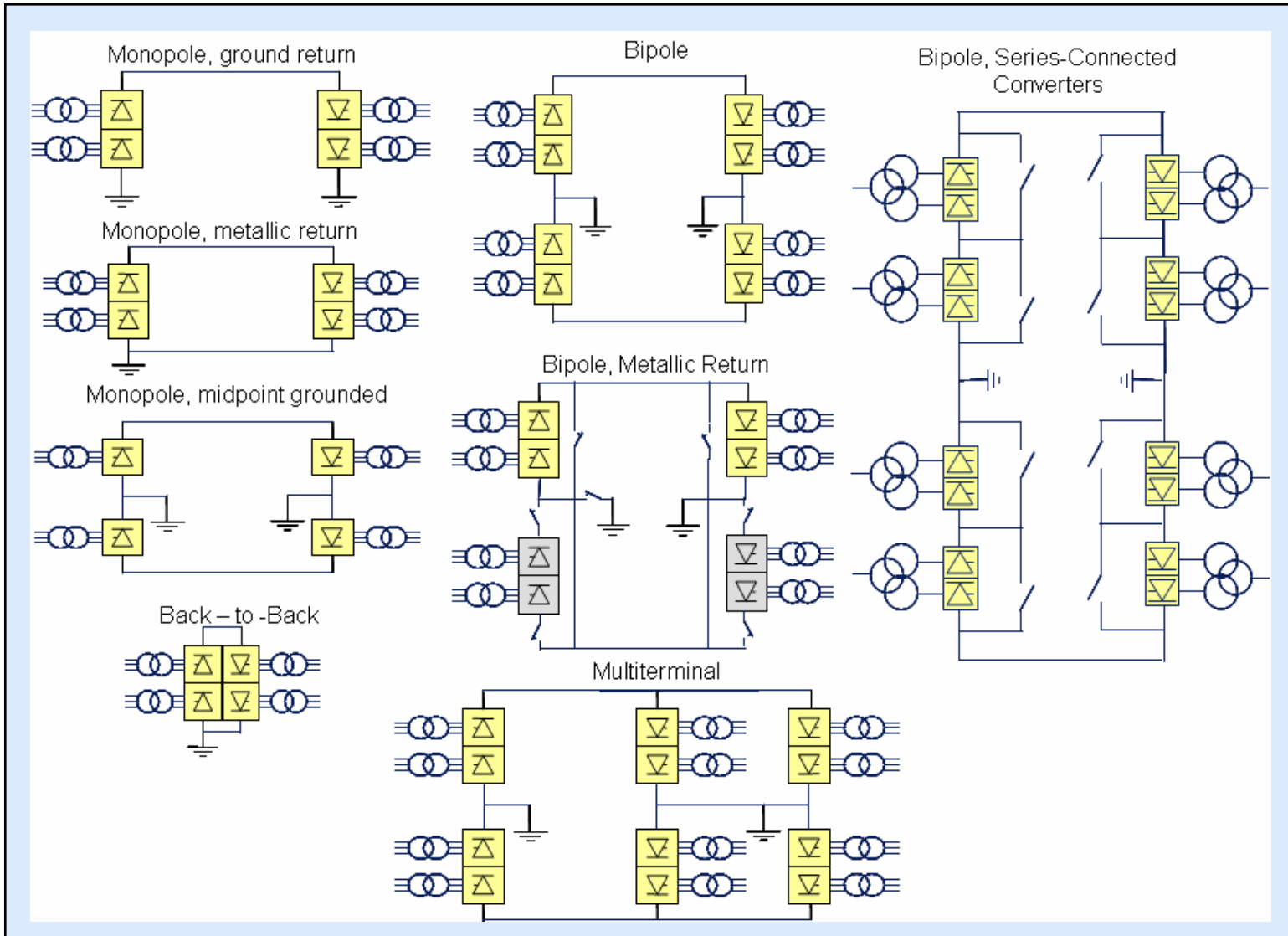
- Thyristor valves
- Thyristor modules
- Thyristors
- Line commutated



HVDC Light

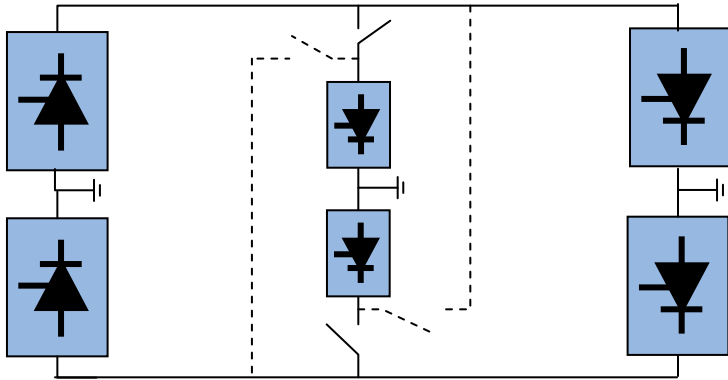
- IGBT valves
- IGBT valve stacks
- StakPaks
- Submodules
- Self commutated

HVDC Operating Configurations and Modes



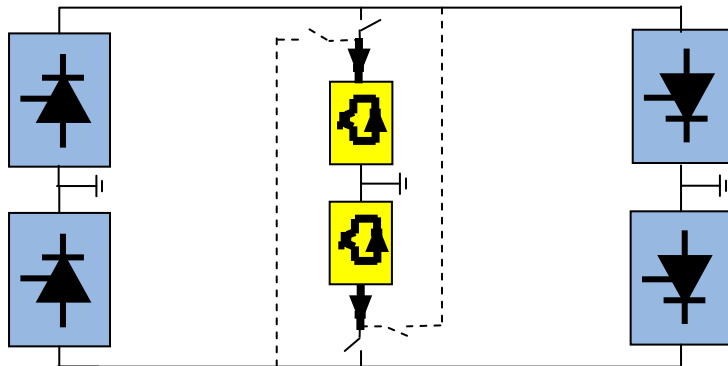
Tapping OVHD HVDC with Large VSC Converters

HVDC Tap



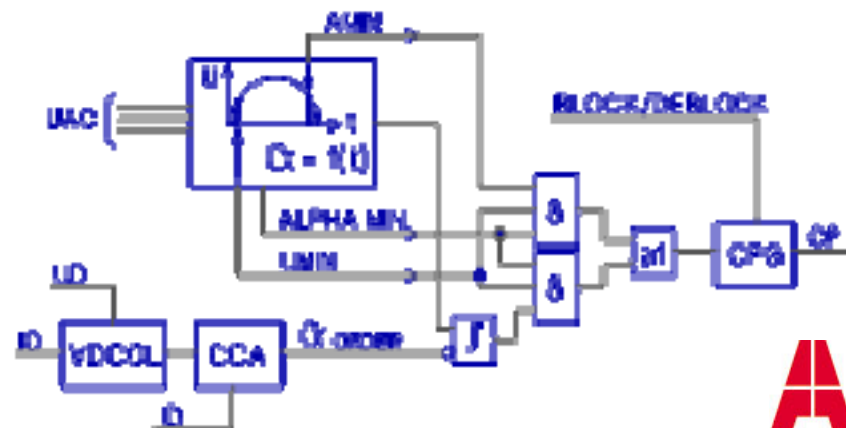
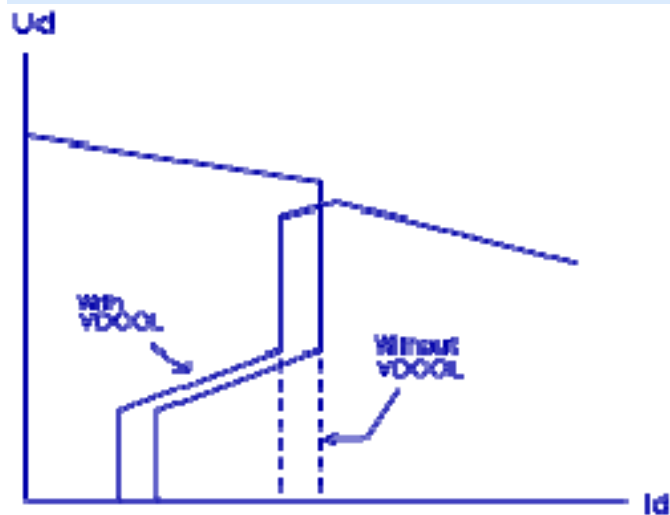
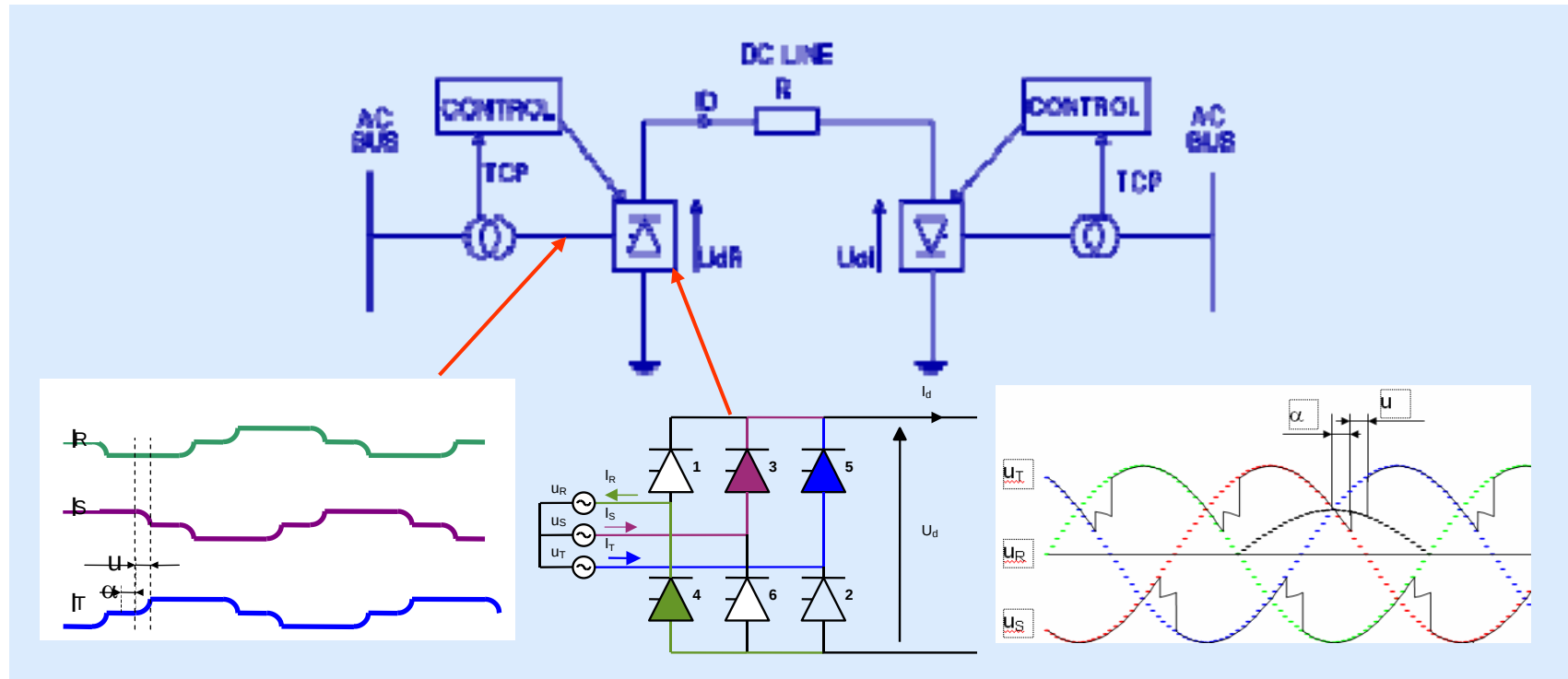
- Reverse power by polarity reversal
- Electronic clearing of dc line faults
- Fast isolation of faulty converters
- Reactive power constraints
- Momentary interruption due to CF at tap
- Limitations on tap rating, location and recovery rate due to stability

HVDC Light Tap

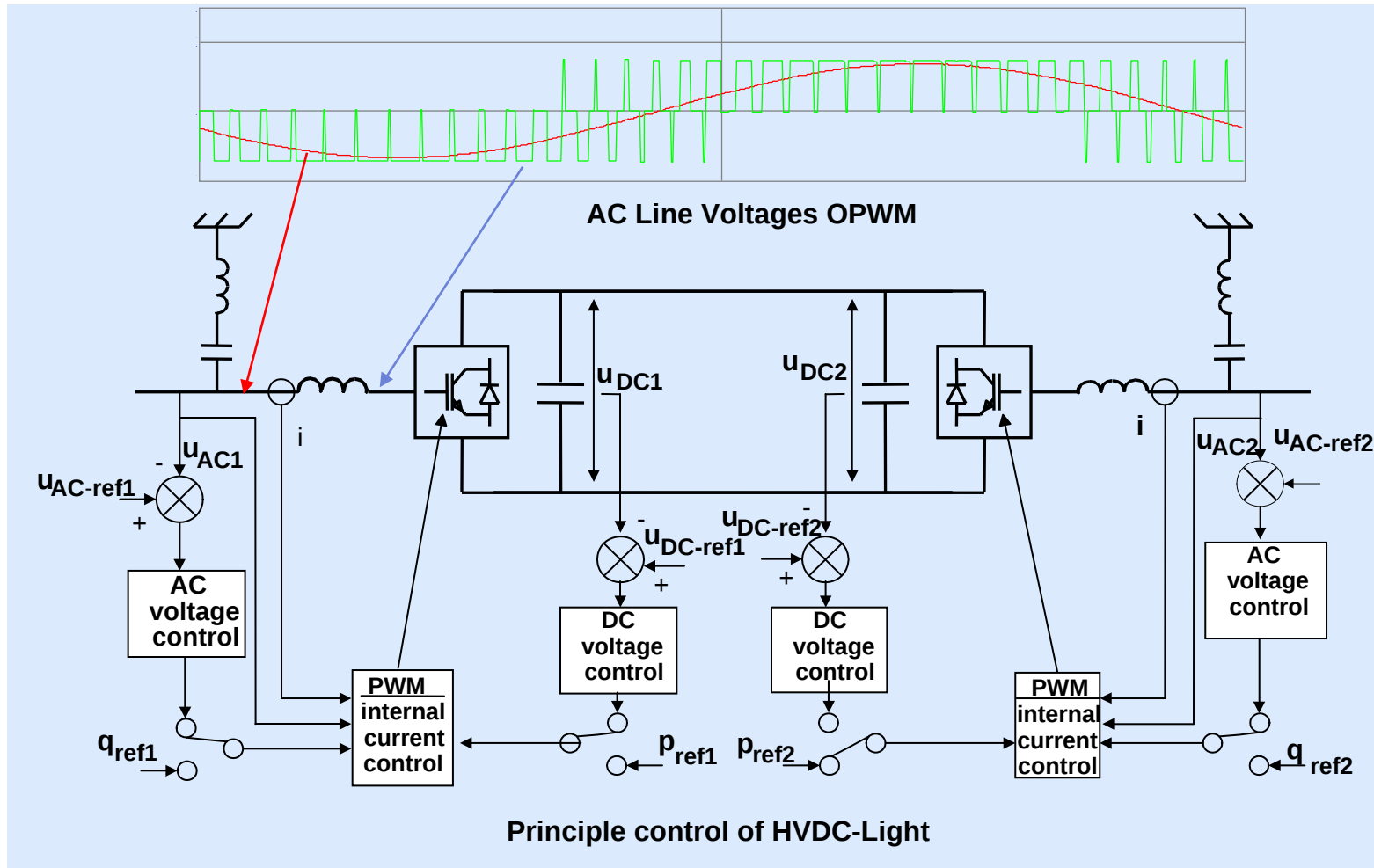


- Polarity reversal if main link is bidirectional
- Cannot extinguish dc line fault current contribution without special provision, e.g., diode coupling for inverter
- No interruption to main power transfer due to CF at tap
- Less limitations on tap rating and location
- Cascade VSC connection for lower tap rating
- No reactive power constraints
- Improved voltage stability

HVDC Classic Control



Control of VSC Based HVDC Transmission



Comparison - AC, HVDC, HVDC CCC and HVDC Light

Attributes	AC Cable	HVDC - Conventional	HVDC – Capacitor Commutated	HVDC Light
Power flow control	None unless PST or series reactor	Continuous $\pm 0.1P_r$ to $\pm P_r$	Continuous $\pm 0.1P_r$ to $\pm P_r$	Continuous 0 to $\pm P_r$
Reactive power demand	$3 I^2 X$ - $3 V^2 B$	Reactive power demand = 50% power transfer	Reactive power demand reduced by series cap	No reactive power demand
Reactive power compensation & control	Shunt reactors	Switched shunt banks 35% in filters + 15% in capacitors	Filters + series compensation of $3 I^2 X_{cc}$	STATCOM + 15% in fixed filters
AC voltage control	Static	Slow - switched filters, capacitors & reactors + LTC	Slow - switched filters, capacitors & reactors + LTC	Dynamic – virtual generator
Voltage stability	Dependent on P, Q and Z	Degraded, special control	Improved, CF lower probability	Superior, no CF
AC system limitation	Cable derated with distance by charging current	Min SCC > 2x converter rating	Min SCC > 1.3x converter rating	None – black start, passive load, induction generators OK



Running Underground

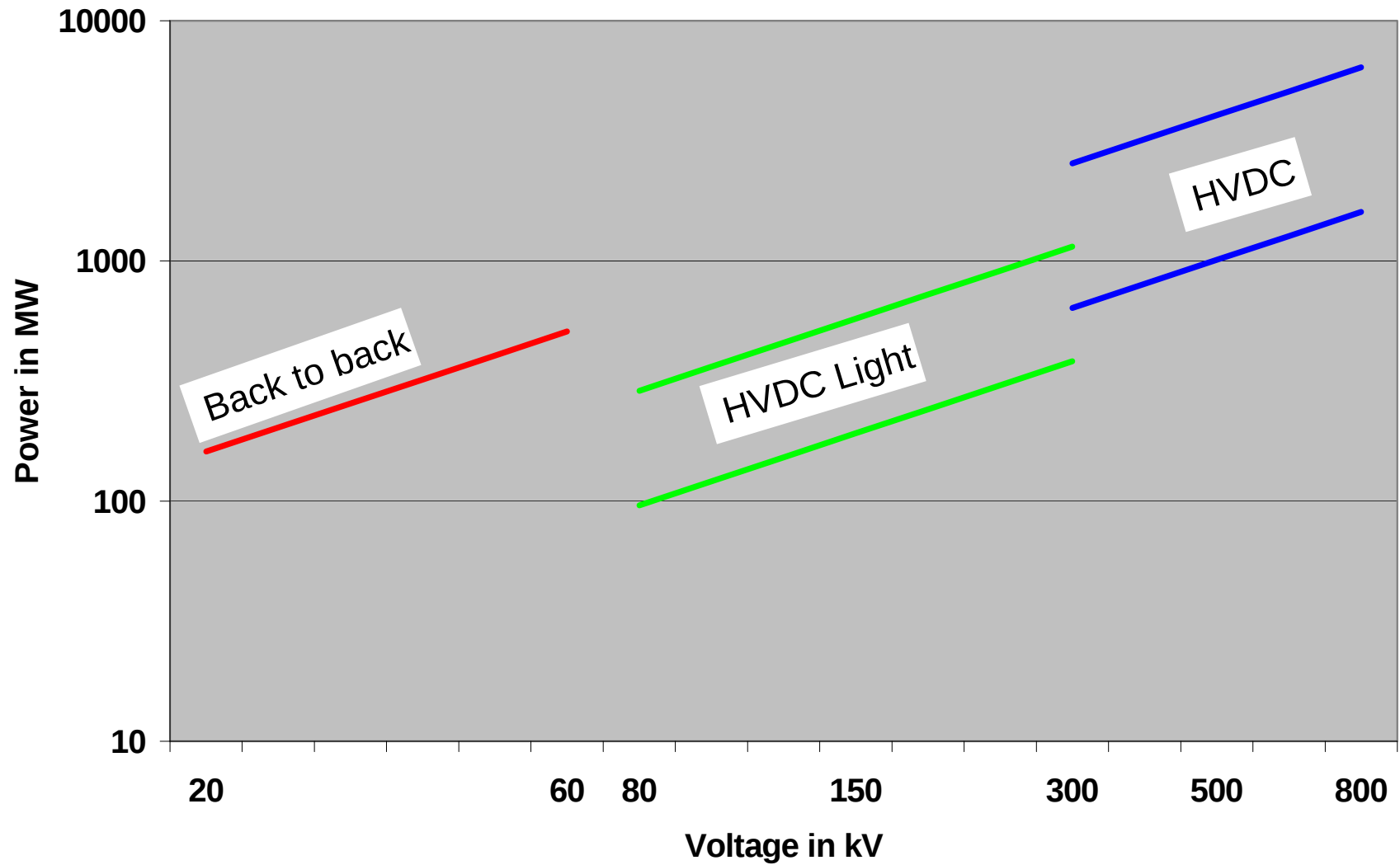


500 kV EHV
1500 MW

$\pm$ 500 kV HVDC
3000 MW

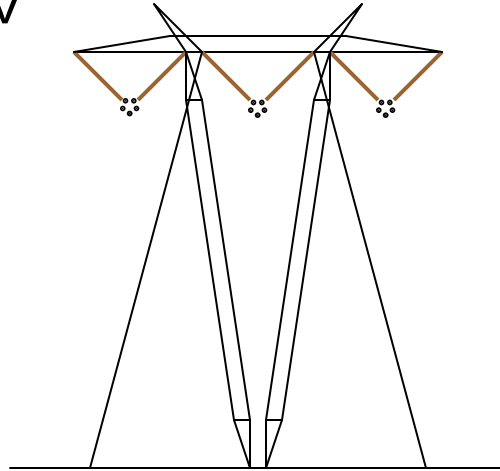
$\pm$ 320 kV HVDC Light
1000 MW

Power Ranges HVDC-Classic and HVDC-Light

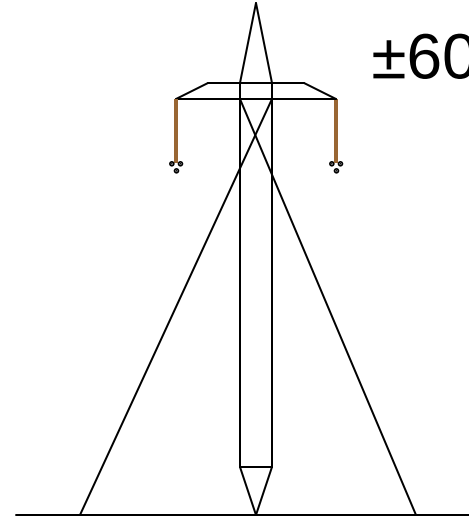


Comparison of overall line design

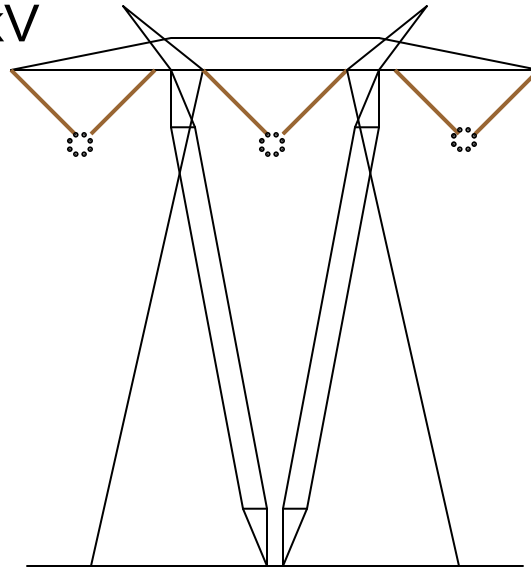
800 kV



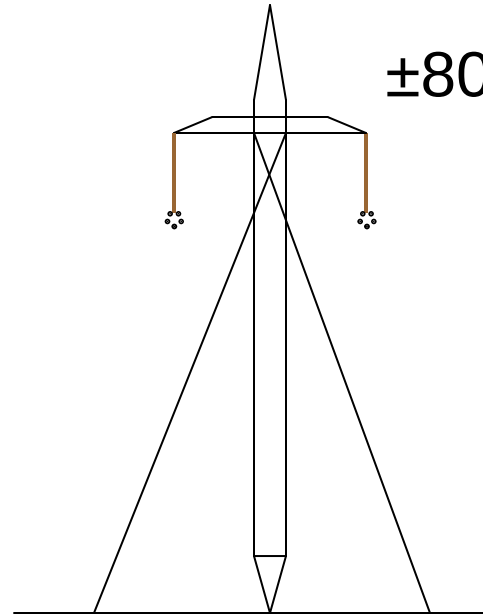
± 600 kV



1000 kV



± 800 kV



Itaipu 765 kV AC Line Performance

	765 kVac Transmission Lines								
	Line 1			Line 2			Line 3		
	Trans	Perm	Length	Trans	Perm	Length	Trans	Perm	Length
1995	0	4	891	1	11	891	-	-	0
1996	1	13	891	0	7	891	-	-	0
1997	0	6	891	2	13	891	-	-	0
1998	0	10	891	2	16	891	-	-	0
1999	1	27	891	1	10	891	-	-	0
2000	3	15	891	3	14	891	2	9	602
2001	2	4	891	4	8	891	2	5	915
2002	4	12	891	1	7	891	4	16	915
8 year	11	91	7128	14	86	7128	8	30	2432

Trans = 0,198 faults / 100km / year

Perm = 1,240 faults / 100km / year

Trans = Successful reclose, one attempt

Perm = Permanent, excluding tower failures

Isokeraunic Level 90 (Foz) to 50 (SP)

Note: “,” = “.”

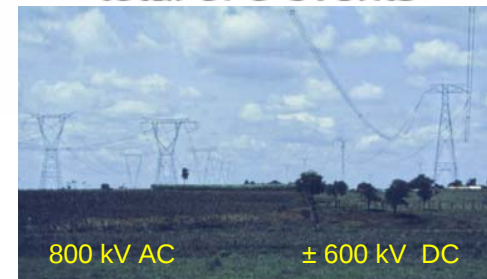
Tower Failures due to wind:

1994 3 both circuits*

1997 2 both circuits*

1998 2 both circuits*

*total of 3 events



ABB

Itaipu 600 kV HVDC Line Performance

	Bipole 1						Bipole 2					
	P1 -			P2 +			P3 -			P4 +		
	Trans	Red.V	Perm	Trans	Red.V	Perm	Trans	Red.V	Perm	Trans	Red.V	Perm
1993	0	1	0	8	1	2	2	0	3	2	0	0
1994	3	0	3	3	0	1	1	2	3	3	0	1
1995	4	0	0	3	0	1	0	0	0	3	1	0
1996	3	0	0	5	0	0	0	0	0	5	0	0
1997	5	2	5	0	0	1	0	0	1*	2	0	1*
1998	2	1	0	4	2	2	0	0	1*	1	0	1*
1999	2	0	0	3	0	0	2	0	1	2	0	1
2000	5	0	1	7	0	1	2	0	0	3	0	0
8 year	24	4	9	33	3	8	7	2	7	21	1	2
Ave.	3	0,5	1,13	4,13	0,38	1	0,88	0,25	0,88	2,63	0,13	0,25

Trans = 0,659 pole faults / 100km / year

RedV = 0,078 pole faults / 100km / year

Perm = 0,202 pole faults / 100km / year

*Line Tower Failures
total two events

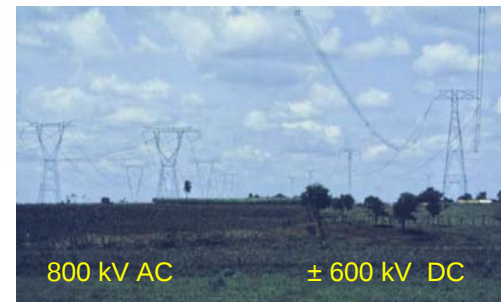
Isokeraunic Level 90 (Foz) to 50 (SP)

Trans = Successful restart at full voltage

RedV = Successful restart at reduced voltage (450 kV)

Perm = Permanent, excluding tower failures

Note: “,” = “.”



ABB